



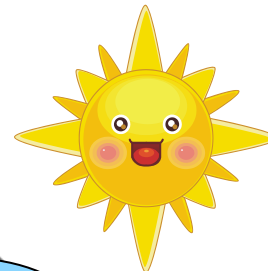
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Mitigating Excessive Pitch and Roll Motions for Semi-Submersibles

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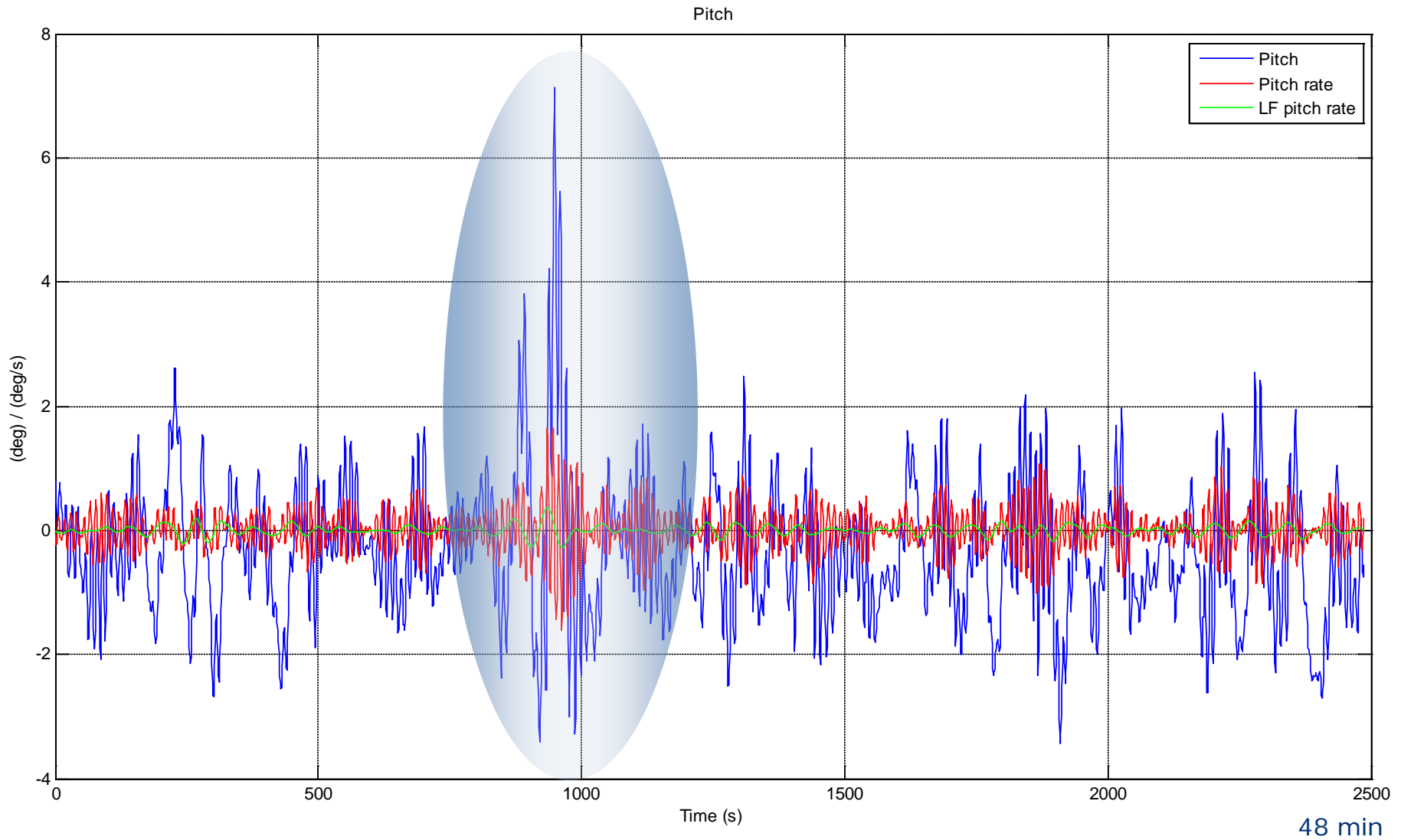
Background

- Observed large pitch and roll motions on (some) new 6. generation drilling rigs
- Natural pitch and roll periods significantly longer than for previous generation semis
- Resonance between hull and mooring in shallow waters
- Thrusters may amplify natural pitching and rolling

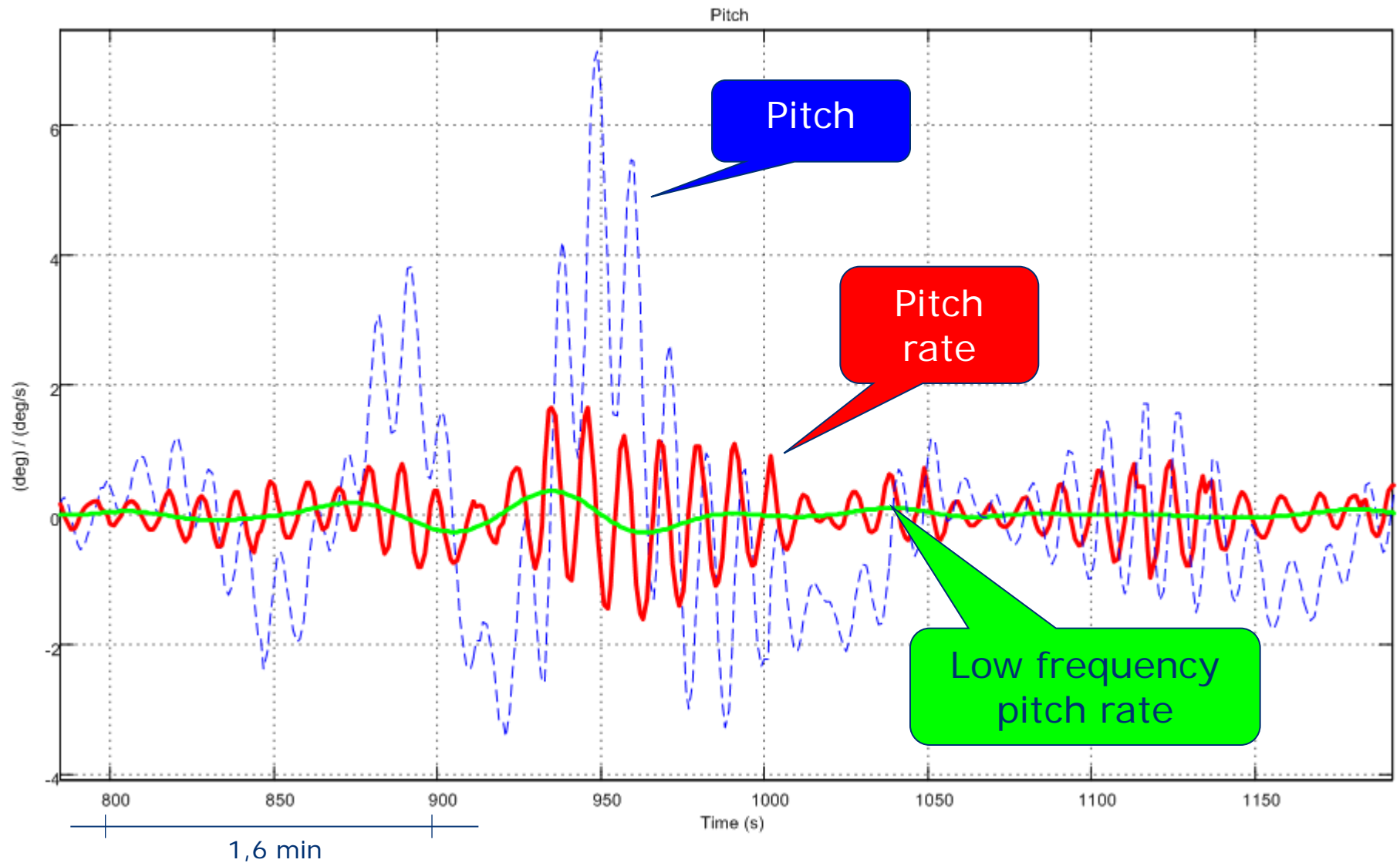


- Can problems be mitigated by using the thrusters?
- Is pitch and roll rate feedback control feasible?

Recorded pitch motion

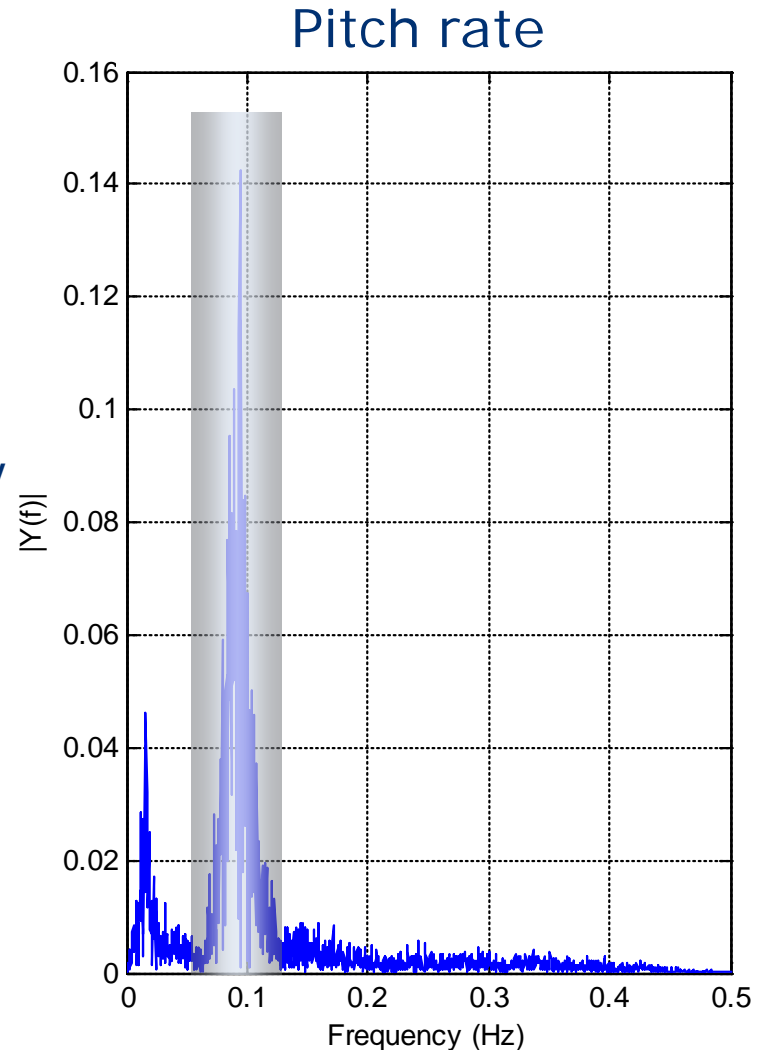


Recorded pitch motion

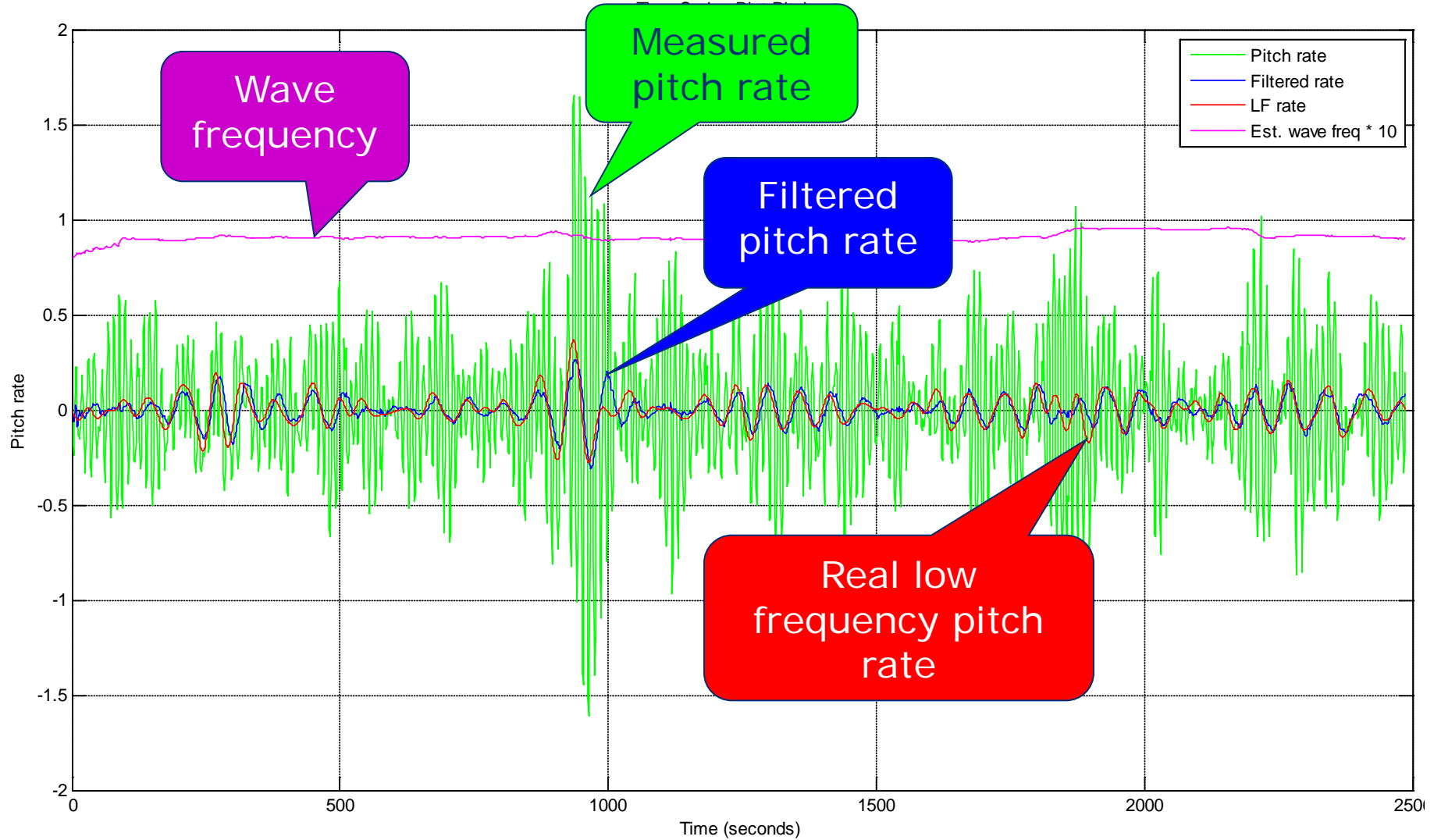


Pitch rate control

- Observations:
 - Wave period ≈ 10 sec
 - Natural oscillation period ≈ 50 sec
 - Wave motion dominant
- Pitch rate signal can not be used for control directly
- Need to filter out wave frequency components
- Dual oscillator filter
 - Natural oscillation period
 - Wave period
 - Adaptive to changing wave characteristics



Adaptive wave filtering



Vessel dynamics

- Pitch – surge motions are dynamically coupled

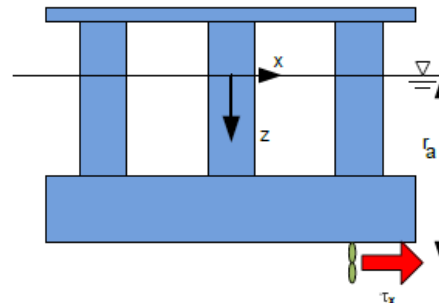
$$\begin{aligned}
 m_{11}\dot{u} + m_{15}\dot{q} + d_{11}u &= \tau_x \\
 m_{51}\dot{u} + m_{55}\dot{q} + d_{55}q + g_{55}\theta &= \tau_x r_a
 \end{aligned}$$

where

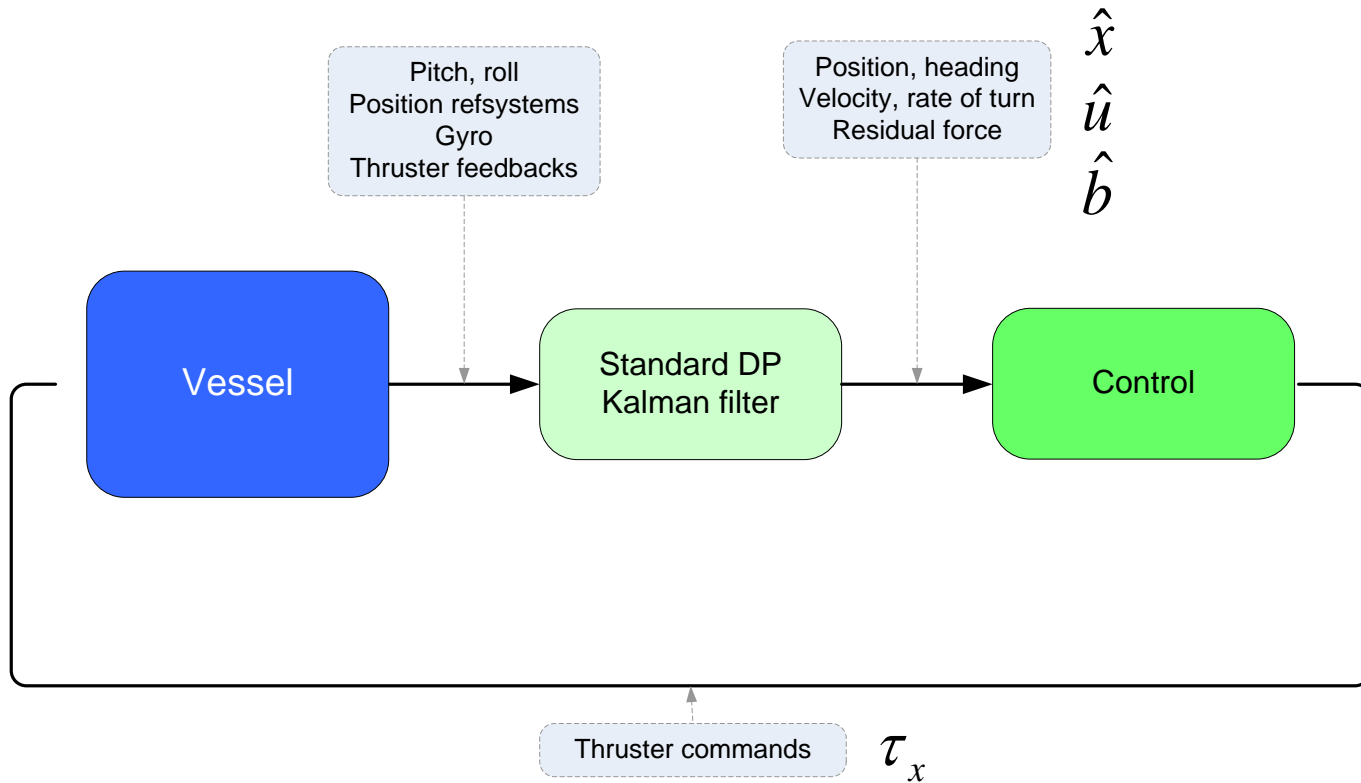
- u surge velocity
- q pitch rate
- θ pitch angle
- m inertia parameters
- d damping parameters
- τ Thrust

Mechanical coupling

Hydro dynamical coupling



Control

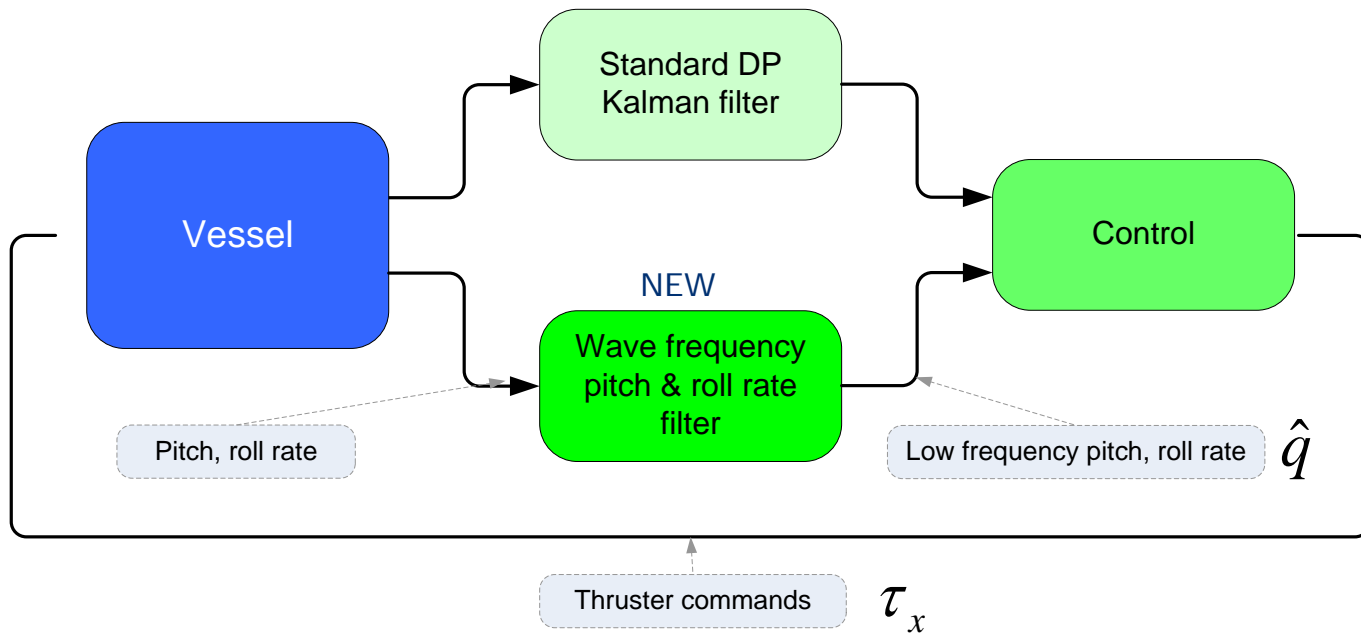


Thrust command

$$\tau_x = -g_{21}\hat{x} - g_{22}\hat{u} + \hat{b}$$

- \hat{x} Low frequency surge position
- \hat{u} Low frequency surge velocity
- \hat{b} Estimated residual forces

Control



Thrust command

$$\tau_x = -g_{21}\hat{x} - g_{22}\hat{u} + \hat{b} - g_{51}\hat{q}$$

- \hat{x} Low frequency surge position
- \hat{u} Low frequency surge velocity
- \hat{b} Estimated residual forces
- \hat{q} Low frequency pitch rate

Simulation example

- Vessel and DP system is simulated

$$m_{11}\dot{u} + m_{15}\dot{q} + d_{11}u = \tau_x + \delta$$

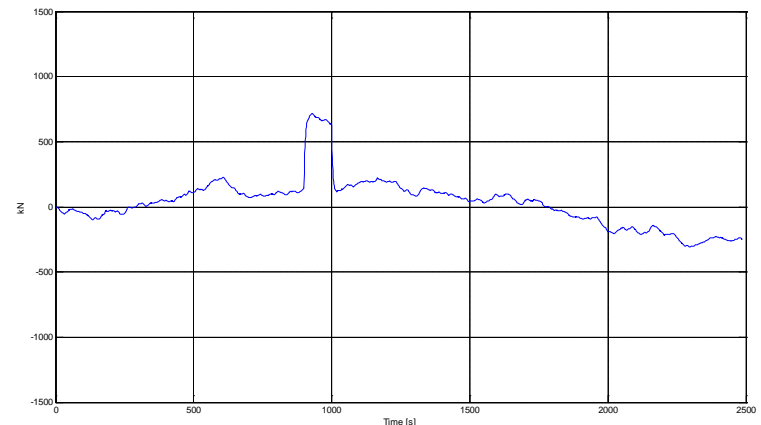
$$m_{51}\dot{u} + m_{55}\dot{q} + d_{55}q + g_{55}\theta = (\tau_x + \delta)r_a$$

$$\tau_x = -g_{21}\hat{x} - g_{22}\hat{u} + \hat{b} - g_{55}\hat{q}$$

$$\begin{bmatrix} \hat{x} \\ \hat{u} \\ \hat{b} \\ \hat{q} \end{bmatrix} = \begin{bmatrix} f(\hat{x}, \hat{u}, \hat{b}, \tau_x) & 0 \\ 0 & g(\hat{q}) \end{bmatrix} \begin{bmatrix} x^{measured} \\ q^{measured} \end{bmatrix}$$

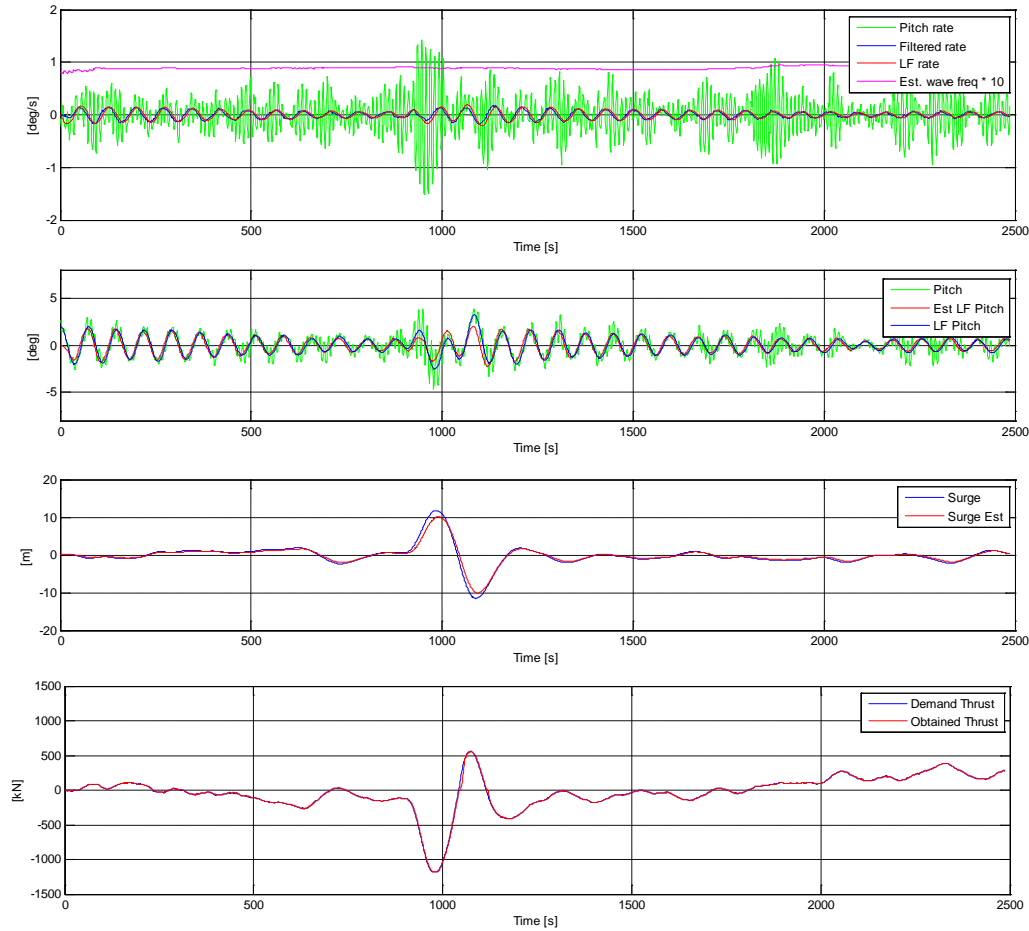
where δ is a disturbance

- slowly varying random value
- pulse 50 tonnes for 100 sec



Normal DP control

- Almost persistent pitching



Pitch rate

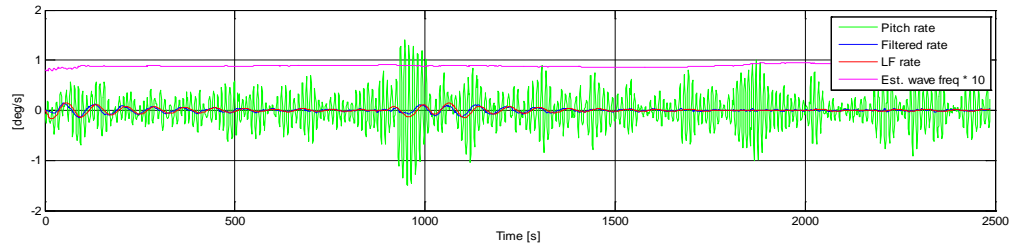
Pitch

Surge

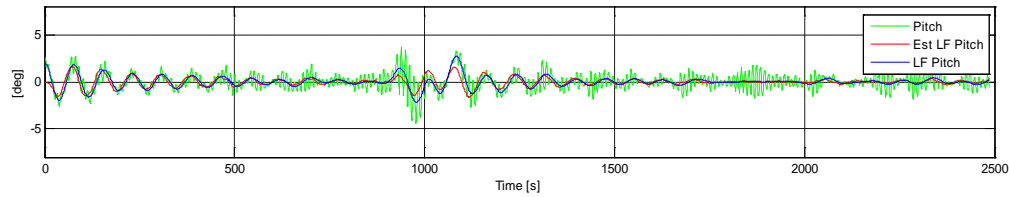
Thrust

DP with pitch rate feedback

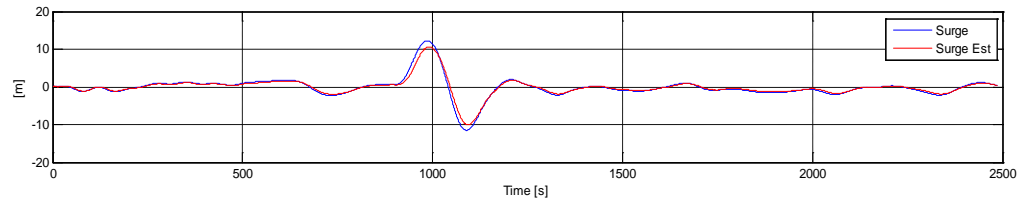
- Well damped pitching



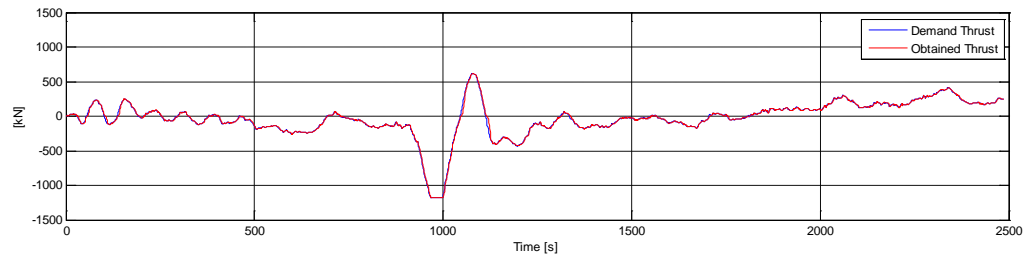
Pitch rate



Pitch



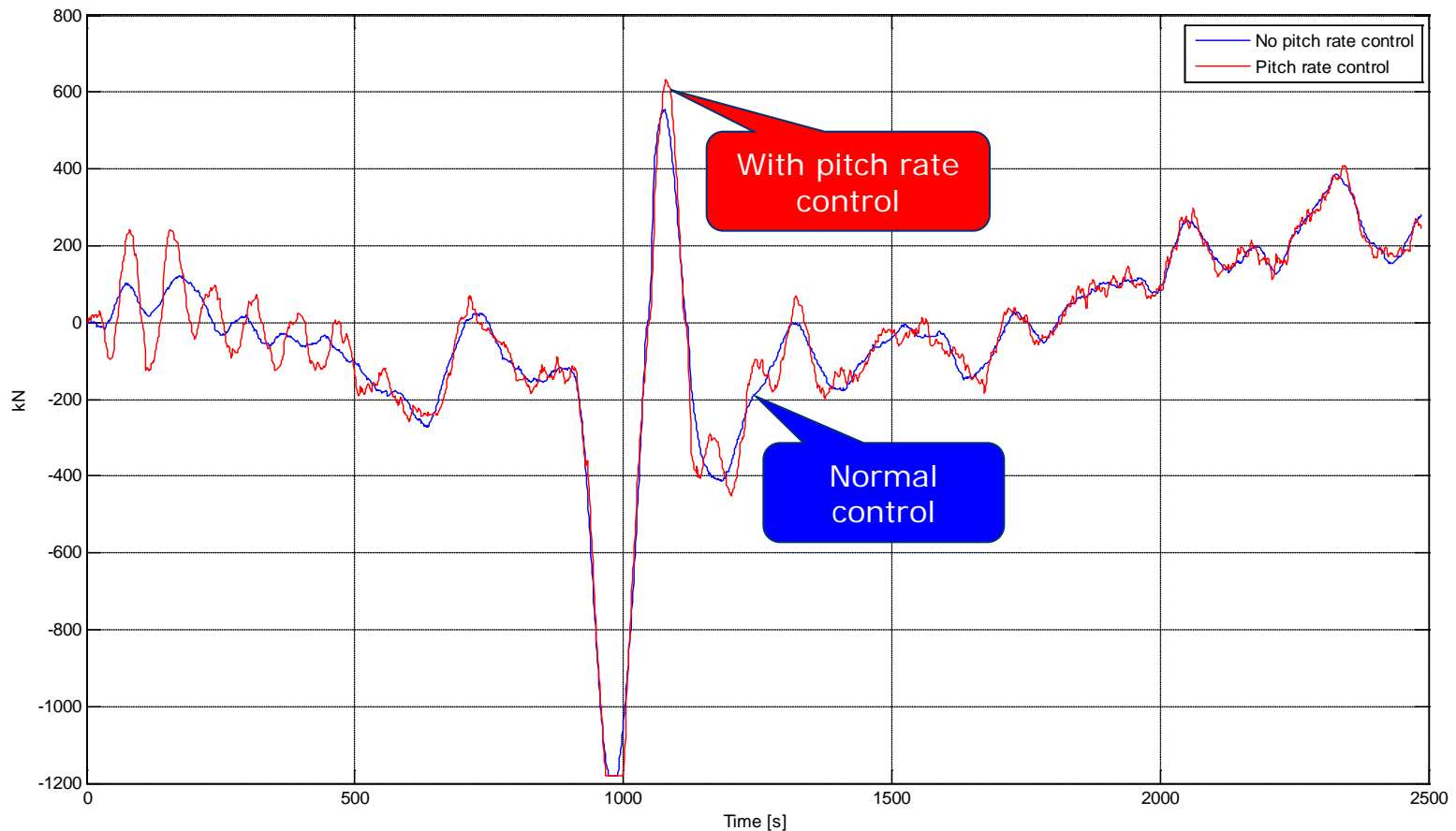
Surge



Thrust

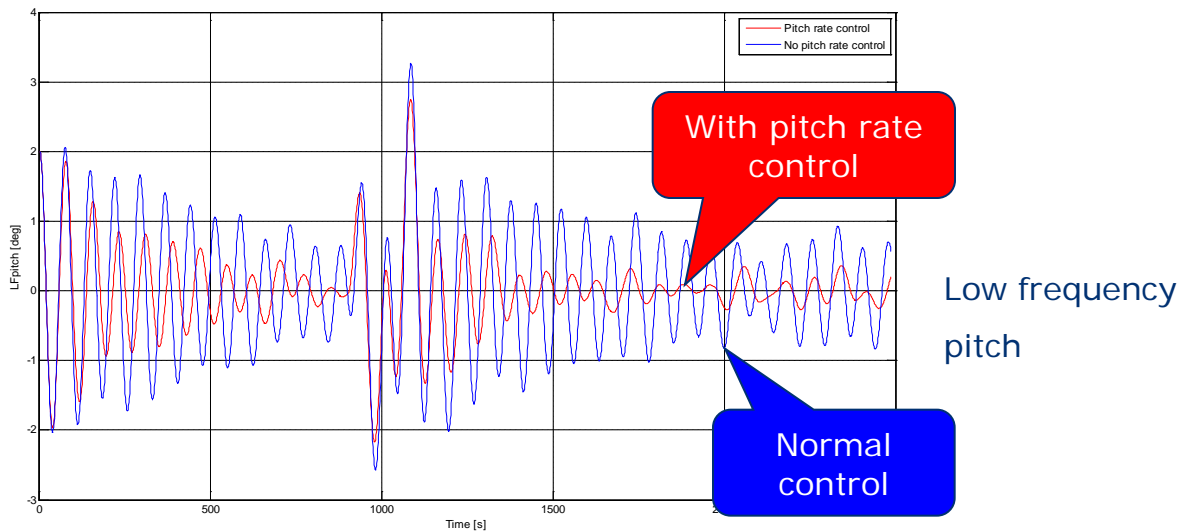
Thruster command details

- Pitch rate control does not require significant additional thrust

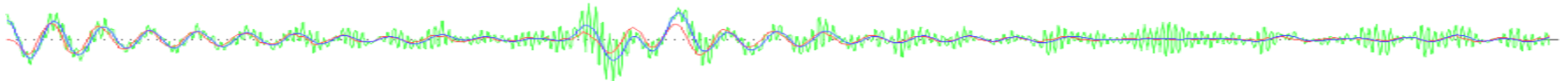


Conclusions

- The overall pitching and rolling can be reduced
- A significant damping of the low frequency pitch and roll motions may be expected
- For sudden external excitation the pitch rate control can not significantly improve the immediate transient pitching but will dampen the effect over time
- No improvements can be expected for the wave frequency components



Thank you for your attention
Questions?



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